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EXPLORATION REPORT

IRON, METAL, RECOVERED IN THE REPUBLIC OF THE CONGO,  
BELIEVED TO BE AN UNIDENTIFIED FLYING OBJECT  
(COUNTRY UNIDENTIFIED) (U)

MN-25500

SECTION I. (C) Purpose (U)

1. (C) The purpose of this report is to present the results of the exploitation of a metallic fragment recovered near the town of Kereleze in the Republic of the Congo. The recovery was the result of a ground-level search which was conducted after an unidentified flying object exploded and fell to earth in the area. The sighting and recovery took place sometime between 10 and 15 October 1963. Other than a reported east-to-west direction of flight for the UFO, specific observation and recovery details are lacking.

SECTION II. (C) Description (U)

2. (C) Details concerning the exact location and characteristics of space are unknown. However, the appearance of the fragment indicated exposure to high temperatures prior to impact (U). The impact of the specimen had little or no effect on its physical condition or appearance. The fragment weighed 16.11g. and had an indefinite density of approximately 7.7 g/cm<sup>3</sup>. The fragment was approximately 2.23 ± 1.73 = 1.0 inches. The top and side views of the specimen were rounded and appeared to have been shaped by heating and melting. This is illustrated in Figures 1 and 2. The top curved groove, visible in Figure 1, is the outline of an insert of metal that differs markedly from the rest of the specimen. Figure 3 shows the side view of the specimen.

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and was composed of six machined or formed rectangular fins extending along the major axis of the fragment.

SECTION III. (C) Conclusion:

3. (C) The fragment was originally part of an electrical component and could be identified as a motor structure, generator structure, or associated electrical regulator device.
4. (C) The fragment was constructed of 1.10-inch thick silicon steel laminate stacked on a central mild steel core or shaft.
5. (C) Materials, processes, dimensions, etc., as such, prevent determination of exact origin (country).
6. (C) Surface appearance and microstructure of the specimen indicates exposure to temperatures in excess of 2500° F.

SECTION IV. (C) Explosive Use (S)

7. (C) The recovered specimen had a density of 7.8 grams and had a density closely approximated by copper. The presence of copper in the metal as heavy oxide was confirmed. The temperatures in excess of 2500° F. while there are no indications of copper, the recovered metal, as shown in Figures 4 and 7, would substantiate the conclusion that the item was moving at a high velocity when it was broken.

8. (C) Fabrication of the item was determined utilizing more or less standard procedures for fabricating electric motor structures.

A massive laminates were stamped (punched) from approximately 1012-inch thick sheet steel, copper plated, and assembled on a mild steel shaft approximately 1.633 inches in diameter. Following assembly, the laminates were joined by soldering or diffusion-bonding of the copper

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plating. This can be accomplished by tightly compacting the laminate assembly and heating in a furnace. Temperature required for bonding of the copper depends upon the degree compaction or pressure; the higher pressures requiring proportionately lower temperatures.

9. (C) A cross-section (across the 20% length of the specimen) is shown in Figure 5. The light-colored, jagged areas are the edges of individual laminates, caused by cutting at an angle to, instead of parallel to, the laminates. It is noted that the copper fins or petals are "T" shaped. This shape is used to help hold winding wire in place and is found on high RPM motors. The melted condition of some of the "T's" is indicative of the high heating conditions experienced. The outer surface of the armature shaft is serrated to prevent axial slippage of the laminates.

10. (C) The lamination or stacking of individual laminates is clearly illustrated in Figure 6. The separate laminates on the fin at the top of the photograph is due to the melting and flowing of the copper plating during the high temperature exposure of the specimen. Some of the copper has been deposited on the fin at the bottom of the photograph. A magnified cross-section of this area is shown in Figures 7 and 8.

11. (C) Another result of intense heating was the reduced grain size of the steel laminations. The microstructure of the laminates shown in Figure 9, yet 16 millimeter grain sizes that are comparable to Category 2 of MIL-STD-883C.

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intense heat and then cooled at a comparatively slow rate.

12. (C) The light material between the laminations in Figure 9 is plated copper that melted and flowed between the laminations when the entire specimen was hot. A photomicrograph of this is shown in Figure 11.

13. (C) Analysis of the melt disclosed the following:

<u>Element</u>	<u>Percent Present (approx.)</u>
Carbon	less than 0.10
Manganese	0.37
Silicon	less than 0.01
Nickel	less than 0.10
Chromium	25
Molybdenum	(+) 3

14. (C) Chemical composition of the steel laminations was as follows:

<u>Element</u>	<u>Percent Present (approx.)</u>
Manganese	25
Silicon	(+) 3
Nickel	0.17
Chromium	less than 0.01
Molybdenum	less than 0.01

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Figure 1 Top View

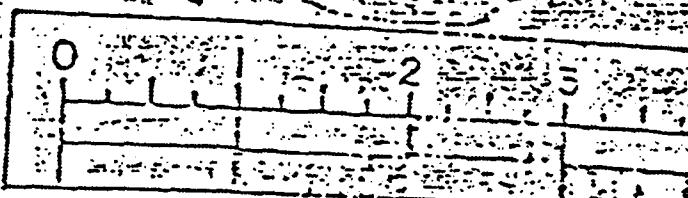


Figure 2 Side View

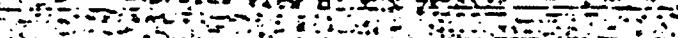


Figure 3 (W) Opposite View of Fig. 5 (L)

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Figure 3. Cross Section (parallel to the  
Length of the Specimen)  
Magnification 21.00

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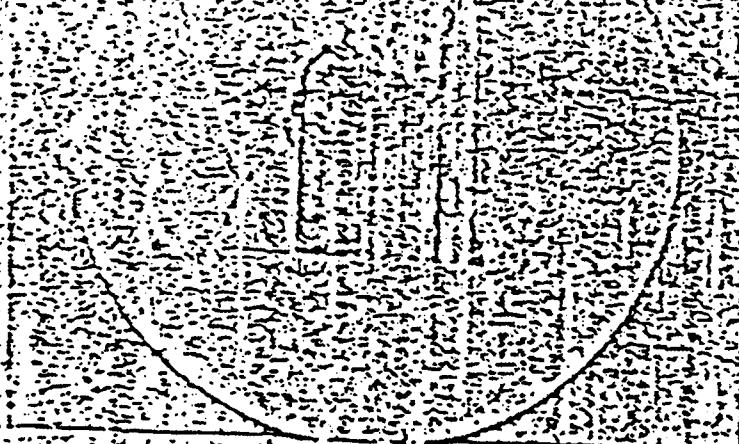


Figure 7. Micrograph Cross-Section of  
Leaded A-rod  
Magnification 3,750 X

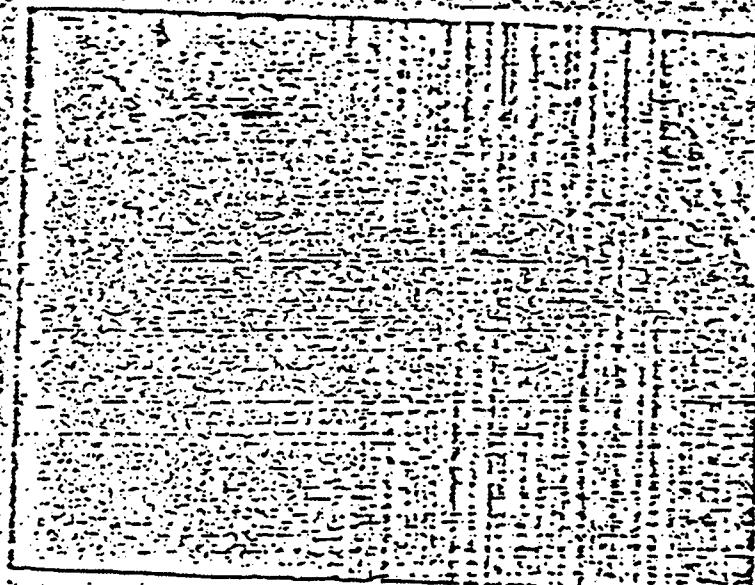


Figure 8. Micrograph Cross-Section of  
Leaded B-rod  
Magnification 3,750 X

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Figure 9 (4) X 100 Picture  
Lat. 1000  
Magnification 65  
(32 Nitral Etched)

